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6.002 Recitation 2020/04/10

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Recitation 8: Impedance, admittance, and graphical representations

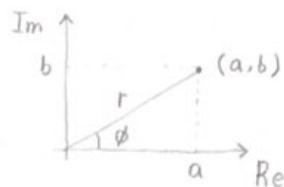
1. Review of complex numbers

$$Z = a + jb$$

\uparrow complex \uparrow real \uparrow imaginary

$$Z = r e^{i\phi}$$

\uparrow magnitude \nwarrow phase



base on the diagram:

$$r = \sqrt{a^2 + b^2} \quad a = r \cos \phi$$

$$\phi = \tan^{-1}\left(\frac{b}{a}\right) \quad b = r \sin \phi$$

$$\text{note: } j^2 = -1, \quad \frac{1}{j\omega} = \frac{j}{j^2\omega} = -j\frac{1}{\omega}$$

2. Impedance

motivation: solving 2nd order differential equations can be tedious. In many scenarios, we are interested in the steady-state solution after the transient solution decays. The method of using impedance formulation is very effective for solving the steady-state behaviors of a circuit when the driving source is sinusoidal.

Impedance describes the relationship between the complex voltage ($V_0 e^{st}$) and current ($I_0 e^{st}$) in a circuit element (e.g. resistor, capacitor, inductor).

$$\text{Defn: } Z = R + jX$$

\uparrow impedance \uparrow resistance \nwarrow reactance

$$Y = \frac{1}{Z}$$

\uparrow admittance

$$Y = G + jS$$

\uparrow conductance \nwarrow susceptance

Let's calculate the impedance of circuit elements:

1. Capacitor

$$i = C \frac{dv}{dt}$$

$$I_0 e^{st} = C \frac{d}{dt}(V_0 e^{st})$$

$$I_0 e^{st} = C s V_0 e^{st}$$

$$\frac{V_0}{I_0} = \frac{1}{Cs}$$

2. Inductor

$$v = L \frac{di}{dt}$$

$$V_0 e^{st} = L \frac{d}{dt}(I_0 e^{st})$$

$$V_0 e^{st} = L s I_0 e^{st}$$

$$\frac{V_0}{I_0} = L s$$

3. Resistor

$$v = R i$$

$$V_0 e^{st} = R I_0 e^{st}$$

$$\frac{V_0}{I_0} = R$$

If we will be using sinusoidal driving sources, let's substitute s with $j\omega$

$$\frac{V_0}{I_0} = \frac{1}{j\omega C}$$

$$\frac{V_0}{I_0} = j\omega L$$

$$\frac{V_0}{I_0} = R$$

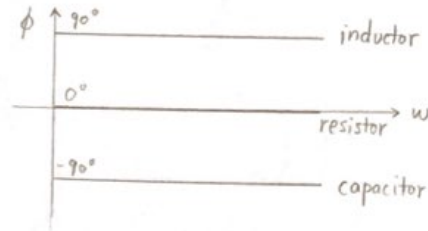
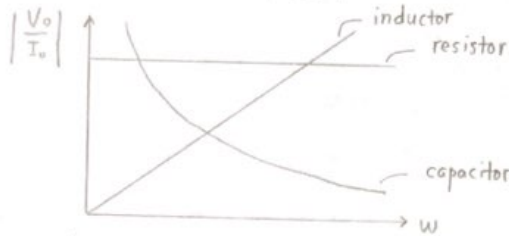
② note that $\frac{V_o}{I_o} \equiv Z$ is a complex number (for an resistor, the imaginary part is 0)
 We can represent the same information with an amplitude and phase.

$$\frac{V_o}{I_o} = \left| \frac{V_o}{I_o} \right| e^{j\phi}$$

Capacitor : $\left| \frac{V_o}{I_o} \right| = \frac{1}{\omega C}$ $\phi = -90^\circ$

Inductor : $\left| \frac{V_o}{I_o} \right| = \omega L$ $\phi = 90^\circ$

Resistor : $\left| \frac{V_o}{I_o} \right| = R$ $\phi = 0^\circ$



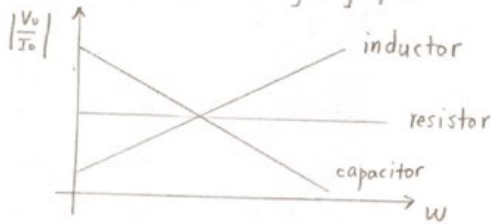
These graphs (amplitude and phase) represent the properties of the circuit elements at different frequencies. What's the behavior at 1Hz? 10Hz? 10000Hz?
 It is beneficial to draw the plots on a log-log or semi-log scale.

capacitor : $\log \left| \frac{V_o}{I_o} \right| = \log \left(\frac{1}{\omega C} \right) = -\log C - \log \omega$

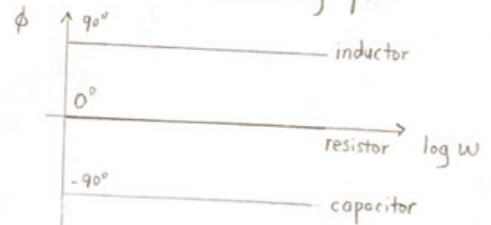
inductor : $\log \left| \frac{V_o}{I_o} \right| = \log \omega L = \log L + \log \omega$

resistor : $\log \left| \frac{V_o}{I_o} \right| = \log R$

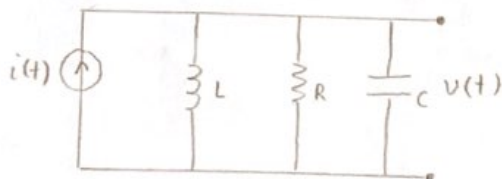
Amplitude on a log-log plot



Phase on a semi-log plot



3. Example : Parallel RLC, sinusoidal response



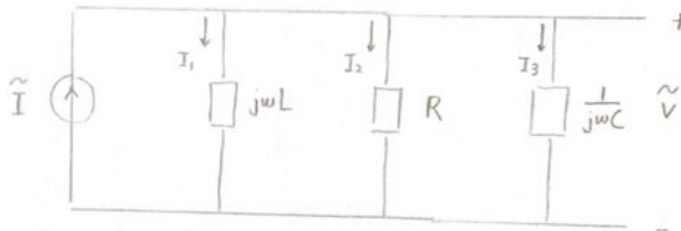
Given the driving source is $i(t) = I_o \cos \omega t$, find the steady state solution $v(t)$

note: we know the steady-state solution $v(t) = V_o \cos(\omega t + \phi)$ has this sinusoidal form, we need to solve for the unknowns V_o, ϕ .

③ We can solve this equation by directly solving the differential equation, but there is an easier approach.

note: $i(t) = I_0 \cos \omega t = \text{Re} [I_0 e^{j\omega t}]$, let's define $\tilde{I} = I_0 e^{j\omega t}$
 $v(t) = V_0 \cos(\omega t + \phi) = \text{Re} [V_0 e^{j\omega t + \phi}] = \text{Re} [V_0 e^{j\phi} e^{j\omega t}] = \text{Re} [V_p e^{j\omega t}]$; $\tilde{V} = V_p e^{j\omega t}$
 note: $V_p = V_0 e^{j\phi}$
 complex

Now let's re-draw the circuit using impedance representation:



apply KCL: $\tilde{I} = I_1 + I_2 + I_3$

$$\tilde{I} = \frac{\tilde{V}}{j\omega L} + \frac{\tilde{V}}{R} + \frac{\tilde{V}}{1/j\omega C}$$

now substitute $\tilde{I} = I_0 e^{j\omega t}$
 $\tilde{V} = V_p e^{j\omega t}$

$$I_0 e^{j\omega t} = V_p e^{j\omega t} \left[\frac{1}{j\omega L} + \frac{1}{R} + j\omega C \right]$$

$$\frac{V_p}{I_0} = \frac{1}{\frac{1}{j\omega L} + j\omega C + \frac{1}{R}}$$

← this is a complex number:

$$\frac{V_p}{I_0} = \frac{1}{\frac{1}{R} + j(\omega C - \frac{1}{\omega L})} \cdot \frac{\frac{1}{R} - j(\omega C - \frac{1}{\omega L})}{\frac{1}{R} - j(\omega C - \frac{1}{\omega L})}$$

$$\frac{V_p}{I_0} = \frac{\frac{1}{R} - j(\omega C - \frac{1}{\omega L})}{\frac{1}{R^2} + (\omega C - \frac{1}{\omega L})^2}$$

Let's find the amplitude and phase information:

$$\left| \frac{V_p}{I_0} \right| = \sqrt{\text{real part}^2 + \text{imaginary part}^2} = \frac{1}{\sqrt{(\frac{1}{R})^2 + (\omega C - \frac{1}{\omega L})^2}}$$

$$\phi = \tan^{-1} \left(\frac{\text{imag}}{\text{real}} \right) = \tan^{-1} \left(\frac{-\omega C + \frac{1}{\omega L}}{1/R} \right)$$

Now we can "read off" the steady-state solution:

$$v(t) = \frac{1}{\sqrt{(\frac{1}{R})^2 + (\omega C - \frac{1}{\omega L})^2}} \cos(\omega t + \tan^{-1} \left(\frac{-\omega C + \frac{1}{\omega L}}{1/R} \right))$$

Note $v(t)$ changes as ω changes, let's plot amplitude and phase:

when $\omega \approx 0$, $\left| \frac{V_p}{I_0} \right| \approx \frac{1}{\infty} = 0$, $\phi \approx \tan^{-1}(\infty) = 90^\circ$

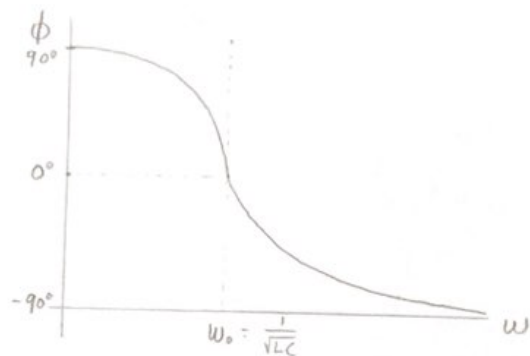
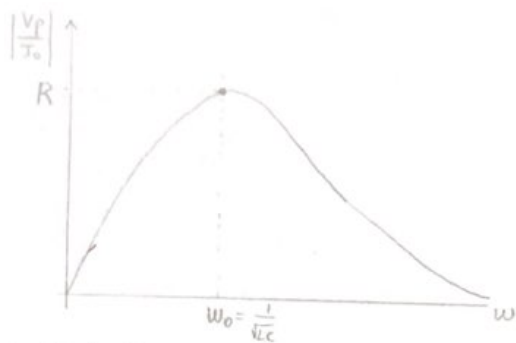
$\omega \approx \infty$, $\left| \frac{V_p}{I_0} \right| \approx \frac{1}{\infty} = 0$, $\phi \approx \tan^{-1}(-\infty) = -90^\circ$

note, when $\omega C = \frac{1}{\omega L}$, $\left| \frac{V_p}{I_0} \right|$ is maximized, $\Rightarrow \omega = \frac{1}{\sqrt{LC}}$ ← natural frequency

when $\omega = \frac{1}{\sqrt{LC}}$, $\phi = \tan^{-1}(0) = 0^\circ$

$$\left| \frac{V_p}{I_0} \right| = R$$

④ We can plot $\left| \frac{V_P}{I_0} \right|$ vs ω , and ϕ vs ω



Let's find the critical angular frequencies ω_1 and ω_2 such that $\left| \frac{V_P}{I_0} \right| = \frac{1}{\sqrt{2}} \left| \frac{V_P}{I_0} \right|$
 solve: $\frac{R}{\sqrt{2}} = \frac{1}{\sqrt{(\omega C - \frac{1}{\omega L})^2 + (\frac{1}{R})^2}} \Rightarrow$ This is equivalent to $(\omega C - \frac{1}{\omega L})^2 = (\frac{1}{R})^2$

we solve for two cases:

$$\textcircled{1} \quad \omega C - \frac{1}{\omega L} = \frac{1}{R} \Rightarrow \omega^2 - \omega \frac{1}{RC} - \frac{1}{LC} = 0 \quad (\text{substitute } \alpha = \frac{1}{2RC}, \omega_0 = \sqrt{\frac{1}{LC}})$$

$$\omega^2 - 2\alpha\omega - \omega_0^2 = 0$$

$$\omega = \alpha \pm \sqrt{\alpha^2 + \omega_0^2}$$

we take $\omega_1 = \alpha + \sqrt{\alpha^2 + \omega_0^2}$ because we require $\omega > 0$

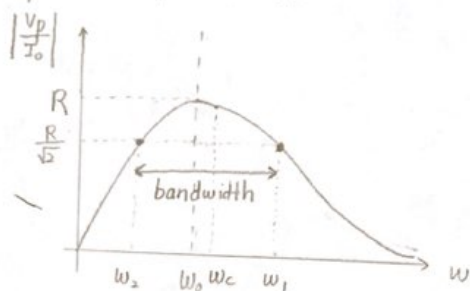
$$\textcircled{2} \quad \omega C - \frac{1}{\omega L} = -\frac{1}{R} \Rightarrow \omega^2 + \omega \frac{1}{RC} - \frac{1}{LC} = 0$$

$$\omega^2 + 2\alpha\omega - \omega_0^2 = 0$$

$$\omega = -\alpha \pm \sqrt{\alpha^2 + \omega_0^2}$$

we take $\omega_2 = -\alpha + \sqrt{\alpha^2 + \omega_0^2}$ because $\omega > 0$

Let's plot ω_1 and ω_2 :



$$\text{note } \omega_1 = \alpha + \sqrt{\alpha^2 + \omega_0^2}$$

$$\omega_2 = -\alpha + \sqrt{\alpha^2 + \omega_0^2}$$

define $\omega_c = \sqrt{\alpha^2 + \omega_0^2} :=$ center frequency

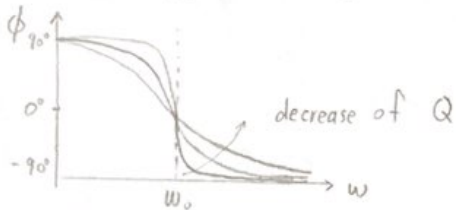
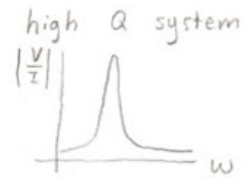
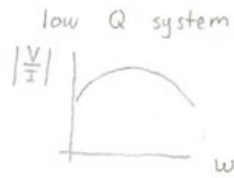
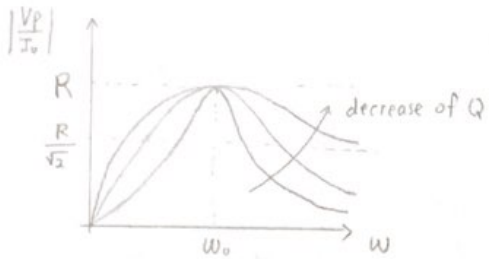
$$\text{bandwidth} = \omega_1 - \omega_2 = 2\alpha$$

Bandwidth is an important concept. It gives the range of frequencies a circuit is responsive to. The circuit responds strongly to a driving signal whose frequency falls in the range of $[\omega_2, \omega_1]$. For driving signals whose frequency is far from $[\omega_2, \omega_1]$, the response magnitude is very small.

Finally, let's look at the quality factor Q . $Q := \frac{\omega_0}{2\alpha}$

Another interpretation of Q is that $Q = \frac{\text{natural frequency}}{\text{bandwidth}}$

5) Given ω_0 remains fixed, how does $|\frac{V_P}{I_0}|$ change when Q changes?

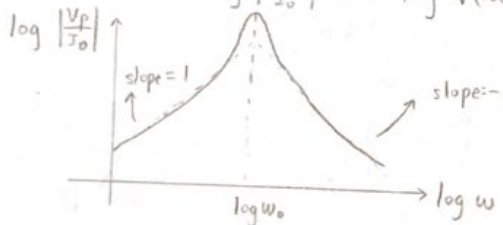


plotting $|\frac{V_P}{I_0}|$ vs w requires a computer program. It is convenient to "sketch" the graph by hand. Log-log plots are easier to sketch

Recall: $|\frac{V_P}{I_0}| = \frac{1}{\sqrt{(\frac{R}{L})^2 + (\omega C - \frac{1}{\omega L})^2}}$ $\Rightarrow \log |\frac{V_P}{I_0}| = -\log \sqrt{(\frac{R}{L})^2 + (\omega C - \frac{1}{\omega L})^2}$

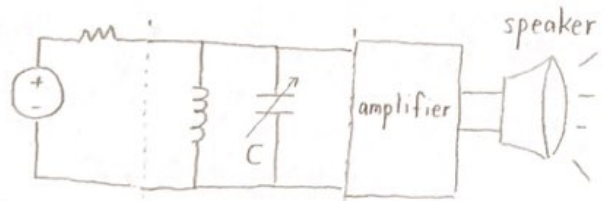
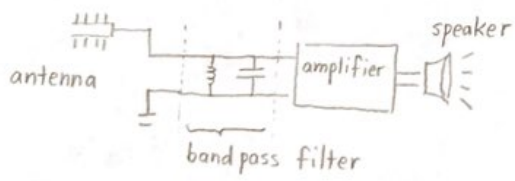
when $w \approx 0$, $\log |\frac{V_P}{I_0}| \approx -\log \sqrt{(\frac{1}{\omega L})^2} = \log w + \log L$ (slope of 1)

$w \approx \infty$, $\log |\frac{V_P}{I_0}| \approx -\log \sqrt{(\omega C)^2} = -\log w + -\log C$ (slope of -1)



* The rate of increase & decay (slopes) is very important for circuit designs

What is this circuit (parallel RLC) good for?
e.g. Amplitude Modulation (AM) Radio Receiver



Antenna + driving source

goal: use the tunable capacitor to select the frequency of interest